



LAWRENCE
LIVERMORE
NATIONAL
LABORATORY

SIMULATION OF CHAMBER TRANSPORT FOR HEAVY-ION FUSION DRIVERS

W. M. Sharp, D. A. Callahan, M. Tabak, S. S. Yu,
P. F. Peterson, D. V. Rose, D. R. Welch

May 20, 2004

Third International Conference on Inertial Fusion Science
Applications
Monterey, CA, United States
September 7, 2003 through September 12, 2003

Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

SIMULATION OF CHAMBER TRANSPORT FOR HEAVY-ION FUSION DRIVERS

W. M. Sharp¹, D. A. Callahan¹, M. Tabak¹, S. S. Yu², P. F. Peterson³, D. V. Rose⁴, D. R. Welch⁴

¹ Lawrence Livermore National Laboratory, Livermore, CA 94550, USA

² Lawrence Berkeley National Laboratory, Berkeley, CA 94720, USA

³ University of California Berkeley, Berkeley, CA 94720, USA

⁴ Mission Research Corporation, Albuquerque, NM 87104, USA

e-mail contact of main author: wsharp@lbl.gov

The heavy-ion fusion (HIF) community recently developed a power-plant design that meets the various requirements of accelerators, final focus, chamber transport, and targets. The point design is intended to minimize physics risk and is certainly not optimal for the cost of electricity. Recent chamber-transport simulations, however, indicate that changes in the beam ion species, the convergence angle, and the emittance might allow more-economical designs.

I. INTRODUCTION

The final transport of a heavy-ion beam to a fusion target poses conflicting demands. Analyses of power-plant economics strongly favor the use of ions with low energy and atomic mass, although this choice requires a higher total current on target, driving up either the number of beams or current per beam. The indirect-drive distributed-radiator targets^{1,2,3} presently preferred for heavy-ion fusion (HIF) require millimeter-sized beam-spot radii on the target ends. This requirement and the need for azimuthally symmetric deposition argue for using many beams, each with low emittance and net charge. Finally, the escape of radiation and neutrons from the target must be minimized to prolong magnet and fusion-chamber lifetimes. These objectives are met in HIF power-plant designs by using jets of molten salt to protect the fusion-chamber walls, although collisional ionization with the resulting background-gas in the chamber complicates beam transport to the target.

A point design meeting these constraints has recently been worked out.⁴ This so-called “robust point design” is deliberately conservative, aiming to minimizing the physics risk rather than the cost of electricity. A pivotal feature of the design is the use of low-density plasma in the beam line between the final-focus magnets and the

chamber to neutralize much of the beam space charge.^{5,6,7} Plasma electrons are trapped in the potential of the passing beam and are carried to the target, allowing substantial beam currents while still maintaining the low net charge needed for good focus.

In this paper, we use the electromagnetic particle-in-cell code LSP^{8,9} to investigate chamber transport of the beams called for in the robust point design. Parameters of the design are reviewed briefly in Section II, and Section III summarizes the results of simulations departing from these point-design parameters in various ways. A concluding section discusses the design space available for more-economical power-plant designs.

II. POINT-DESIGN PARAMETERS

The point design builds up the required power profile by using beams with different durations, currents, energies, and arrival times, as sketched in Fig. 1. A total of 120 beams is specified, divided into five classes. The initial lower-energy part of the profile, called the “foot,” is built up by stacking three types of beam, and the main pulse is formed from two more types. The large number of beams is needed both to keep the current in each beam manageable and to give each type of beam adequate azimuthal symmetry when deposited in the annuli on the target ends.

The point design specifies beams of singly charged bismuth ions (209 amu). To have the required stopping power, bismuth main-pulse ions require an energy of 4 GeV. Foot-pulse energies are 25% lower to compensate for the shorter stopping distance at low temperature. The most challenging beams to transport are the initial foot pulses and the final 48 main pulses. These foot pulses are challenging because they must reach the target without additional neutralization from a photoionized plasma

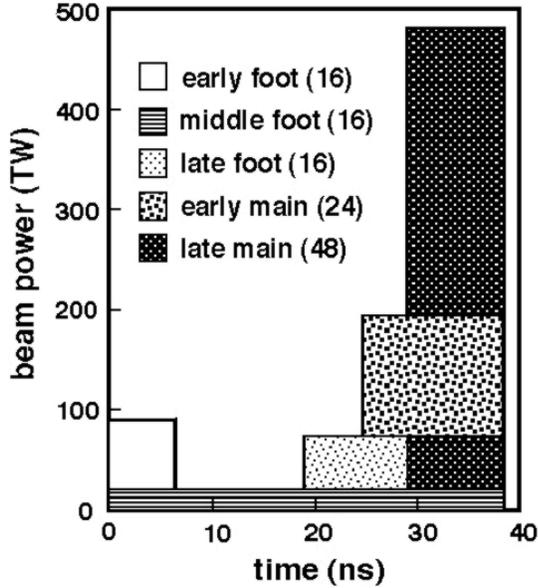


Figure 1 Sketch showing how the power profile can be approximated by constant-current beams with different durations. The number of each type of beam is given in parentheses.

around the target, and the 9.3-ns main pulses are singled out because they have the highest current and perveance¹⁰, which is a measure of the importance of space charge in transverse dynamics. The simulations reported here focus on these two pulse formats. The main pulses have beam current of 2 kA and a perveance of 9×10^{-5} , and the foot-pulse current is 1.5 kA, giving a 7×10^{-5} perveance. In all the cases, the beam current falls off in the 3-ns beam ends like a normal ogive, and the radius drops from its mid-pulse value to 2 cm with a similar S-shaped pattern.

As discussed elsewhere¹¹ in more detail, each beam is focused with a 10-mrad convergence angle on a target location six meters beyond the last final-focus magnet. A beam first passes through a conical 3-m chamber-entry pipe lined with a molten-salt vortex to protect the surface. This molten-salt layer is modeled as an insulator with a surface conductivity of 220 S/m. The beam then enters the 3-m radius fusion chamber, filled with BeF_2 and LiF vapor from the molten salt jets used to protect the chamber walls. This background gas has a vapor pressure of $7 \times 10^{12} \text{ cm}^{-3}$, as is appropriate for thick-liquid walls¹², and the gas density tapers off to zero in the final 50 cm of the beam pipe.

Neutralization after final focus is essential for all the cases discussed here. Analytic work by Olson¹³ indicates that the upper perveance limit for ballistic transport is about 1.6×10^{-5} , so the number of beams would have to be increased more than five-fold to meet this condition. Instead, as in Ref. 11, we use a 10-cm thick plasma layer with a density of $3 \times 10^{11} \text{ cm}^{-3}$ near each end of the 3-m entry pipe to neutralize the beam. This plasma increases beam neutralization near the target from about 30% due to collisional ionization alone to more than 95%.

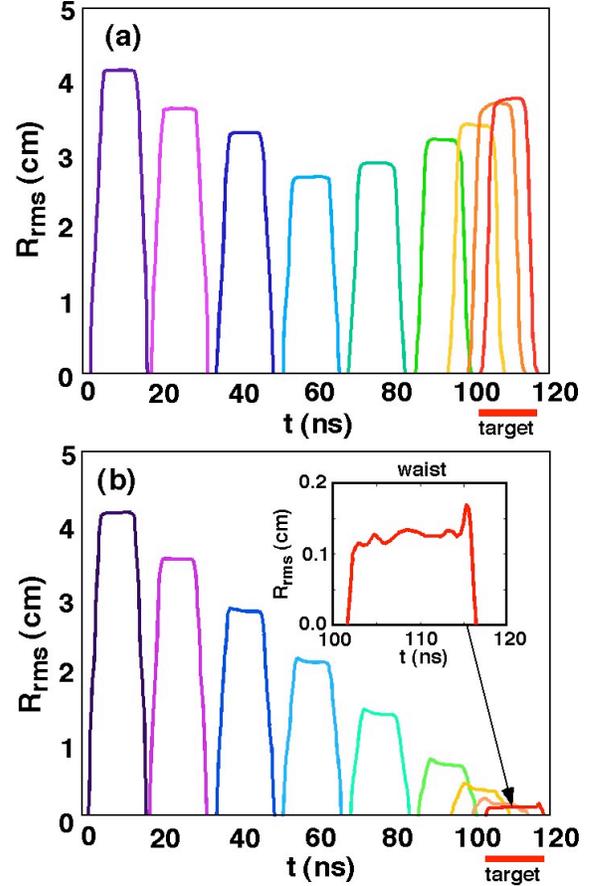


Figure 2. Time variation of a Bi^{+1} main-pulse rms radius at selected axial locations (a) without plasma neutralization and (b) with plasma placed near the ends of the beam-entry pipe

III. RESULTS

In addition to plasma neutralization, the axisymmetric, single-beam simulations here include electron emission from the entry-pipe and chamber walls, collisional ionization of the beam and background gas, and photoionization by X rays from the heated target. Other physical processes, such as collisional scattering and electron emission from the target are omitted because they are found to have no significant effect in trial runs.

III.A Effects of Plasma Neutralization

For the perveance values of the point design, space charge prevents a usable focal spot in the absence of external neutralization. The curves in Fig. 2a show the time variation of the beam root-mean-square (rms) radius at selected axial positions for the 9.3-ns main pulse. The beam minimum radius, or “waist,” occurs after 60 ns of transport, just after the beam has exited the beam port into the chamber, and by the time it reaches the nominal target location, about 100 ns, the radius is larger than the initial value. Although electron emission is allowed from entry-

pipe and chamber wall in this simulation, these electrons are ineffective at neutralizing the beam. Emitted electrons are attracted by the beam space-charge field, gaining an energy that can exceed 10^5 eV. Due to this thermal energy, many of these electrons escape the beam as it converges to the target.

For the same main pulse, adding plasma neutralization produces the greatly improved focal spot seen in Fig. 2b, with an rms radius of about 1.2 mm at the waist. This focal spot meets the target requirement, but the target physics must still be analyzed to ensure that the ions falling outside the intended annulus do not impair the radiation symmetry.

As foot pulses heat an indirect-drive HIF target, soft X rays emitted by the hohlraum photoionize the surrounding background gas. For the gas densities expected in liquid-wall chambers, the resulting plasma improves neutralization near the target for main pulses and the late-arriving foot pulses. This additional neutralization is partly offset, however, by photostripping of the beam and by enhanced collisional stripping by the photoionized background gas. Together, these effects lead to a modest improvement in the beam focal spot. If photoionization is artificially turned off in the case with plasma neutralization here, the focal-spot radius increases by about 10%, even though final emittance is 30% lower without photoionization, and the average charge state drops from about seven to 1.8. The emittance and charge-state increases due to photoionization have only a weak effect on the spot size because they occur too close to the target to affect the beam transverse profile.

For the current used here, magnetic self-pinch is negligible, although it is seen in simulations of beams having initial currents above 4 kA.

III.B Effects of Ion Species

The choice of beam ion species has a major impact on the cost of a driver. Since target stopping power is principally a function of ion velocity, the energy of ions required by a target is approximately proportional to atomic mass M . The cost of induction accelerators increases roughly in proportion to the beam energy, so power-plant studies consistently favor low-mass ions. To test the sensitivity of the beam focal radius to ion mass, we compare beams of xenon (131 amu) with the bismuth results. Since beam current increases inversely with M for a given target, the xenon main pulses must have 3.2 kA of 2.5-GeV ions, and foot pulses require 2.4 kA of 1.9-GeV ions. Beam perveance increases like M^2 , so the corresponding perveance values are 1.7×10^{-4} and 2.3×10^{-4} .

To make a quantitative comparison of these beam species, we note that distributed-radiator targets require that at least 90% of the beam energy be deposited in an annulus on each end of the hohlraum. For the specific target used in the point design, the main pulse must hit an

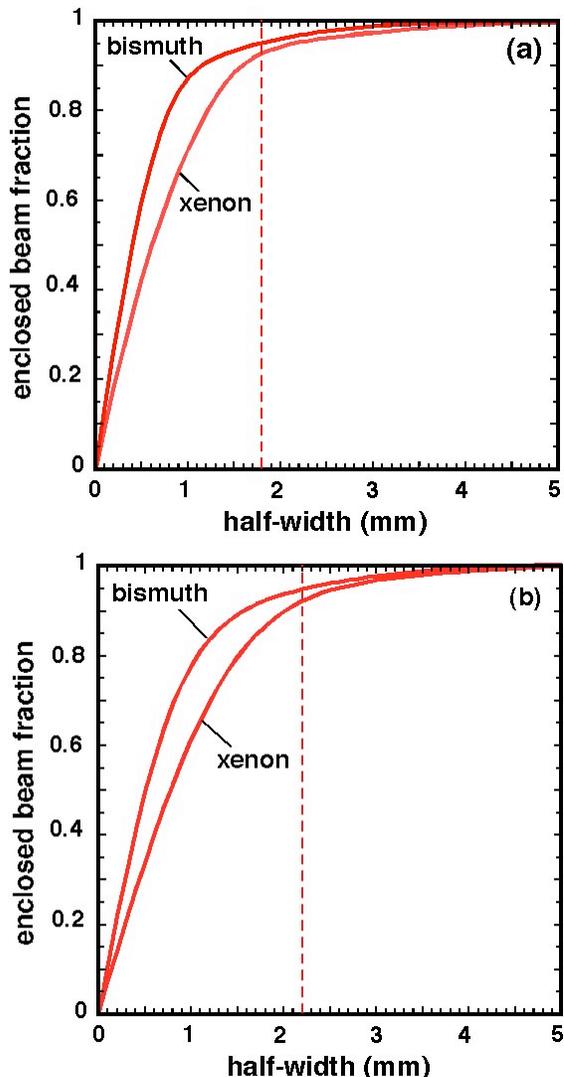


Figure 3. Enclosed current fractions for xenon and bismuth (a) main pulses and (b) foot pulses. The dashed lines show the respective half-widths of the corresponding target annuli.

annulus with a half-width of 1.8 mm, and the annulus for foot pulses has a 2.2-mm half-width. Therefore, a good criterion for evaluating the simulations is the fraction of energy deposited in a band with a half-width equal to that of the target annulus. This measure ignores the curvature of the annulus but is still a useful approximation.

Figure 3a compares the energy deposition for main pulses of bismuth and xenon. While bismuth has better focus near the center of the pulse and is therefore more robust, as expected, both species satisfy the criterion that at least 90% of beam energy falls within the target annulus, shown by a dashed line in the figure. The main pulse fractions are 96% for bismuth and 93% for xenon.

Due to the absence of a photoionized plasma, the foot pulses for the two species have poorer neutralization near

the target, a larger halo, and lower fractional deposition. Nonetheless, the deposition fractions, shown in Fig. 3b, are only about 1% less than the corresponding main-pulse values, due to the wider target annulus.

III.C Effects of Plasma Parameters

The calculated beam focal spots are not sensitive to the density of the neutralizing plasma, provided that the number of electrons in the volume swept out by the beam exceeds the total beam charge. The $3 \times 10^{11} \text{ cm}^{-3}$ plasma density used here is about a factor of ten higher than this minimum, but a significant change in the beam focal radius is only seen when the plasma density is lower than about 10^{10} cm^{-3} . A nearby conducting wall enhances plasma neutralization, however, because image charges on the entry-pipe wall alter the plasma space-charge field and makes it easier to remove electrons along the axis. Child-Langmuir electron emission from the wall further improves beam neutralization by keeping the plasma quasi-neutral as electrons are extracted.

Although the beam focal spot is not sensitive to the plasma density, the axial density profile of the first plasma layer encountered by the beam is found to have a pronounced effect. When the plasma density drops abruptly to zero at the plasma edge, only about 85% of the energy of a bismuth main pulse falls within the requisite 1.8-mm half-width band, but this fraction increases to 92% when the density falls parabolically over 3-cm and to 97% for a 6-cm parabolic or normal-ogive edge. An examination of these cases shows that a current of backstreaming electrons nearly equalling the beam current develops as the unneutralized beam approaches the square-profile plasma. This current flows near the beam axis, and the resulting nonlinear space-charge field within the beam causes a substantial emittance increase. Both the electron current and the emittance increase are less for the other plasma profiles. For example, we see only a 10% emittance increase in the entry pipe for the ogive profile, compared with nearly a doubling for a square plasma edge. For the remaining cases here, we use the more realistic ogival edge profile.

Sensitivity of the beam focal spot to the length of the neutralizing plasma has also been studied. Specifically, we have compared placing a plasma layer near each end of the entry pipe against backfilling the entire entry pipe with plasma. In both cases, each plasma end is modeled by a 6-cm ogival profile, and the same $3 \times 10^{11} \text{ cm}^{-3}$ interior density is specified. For both bismuth and xenon main pulses, a plasma backfill increases the energy deposited on the target annulus by about 3%. Nonetheless, we use the layout with two plasma layers for other cases here because it poses fewer engineering problems.

III.D Effects of Initial Emittance

The robust point design specifies an initial normalized edge emittance of about 2 mm-mrad, allowing less than a factor of five growth from source to target. Simulations show a marked degradation in the beam focal spot when this stringent condition is not met. When the initial emittance of a xenon main pulse is doubled, for example, the energy deposited in a 1.8-mm half-width band drops from 96% to 90%, and this fraction drops to about 85% when the emittance is tripled. Bismuth beams are somewhat less sensitive to emittance change, but a tripling of the nominal value still leads to an unusable focal spot. Since the emittance grows only about 20% in the chamber when a realistic plasma density profile is used, emittance growth in the accelerator is tightly constrained.

III.E Effects of Convergence Angle

A smaller beam convergence angle is preferable for several reasons. The unshielded solid angle around the target through which neutrons, gamma rays, and debris can escape is proportional to the square of the beam radius, so reducing the convergence angle simplifies shielding. In addition, the beam bundle converging on each end of the hohlraum can have a smaller cone angle, allowing the use of higher-gain targets as well as smaller and less costly final-focus magnets.

The robust point design specifies a nominal convergence angle of 10-mrad, corresponding to a 6-cm radius after final focus, six meters from the target. Both bismuth and xenon simulations show less than a 5% drop in the energy deposited within the target annulus when a 7.5-mrad convergence angle is used. This change is substantially less than the 25% predicted from a simple ballistic-transport model, indicating that residual space charge still plays a role in transverse dynamics. Due to this insensitivity to convergence angle, an optimized design would likely use a smaller value, although the other simulations here use 10-mrad.

III.F Effects of Initial Charge State

Recent work on beam sources indicates that intense beams of negatively charged halogen ions may be feasible.¹⁴ Such beams could be photoneutralized after final focus by a laser and would not need a neutralizing plasma. We have simulated chamber transport of a neutral iodine (127 amu) main pulse with the same beam power stopping distance as the point design, so the particle current is 3.3 kA and the energy is 2.4 GeV. For comparison, we also simulated a plasma-neutralized case with I^{-1} and an unneutralized I^{-1} case. The results are shown in Fig. 4. Near the target, the net charge of the iodine beam is less than that of the plasma-neutralized I^{-1} beam, and the fraction of energy deposited in a 1.8-mm

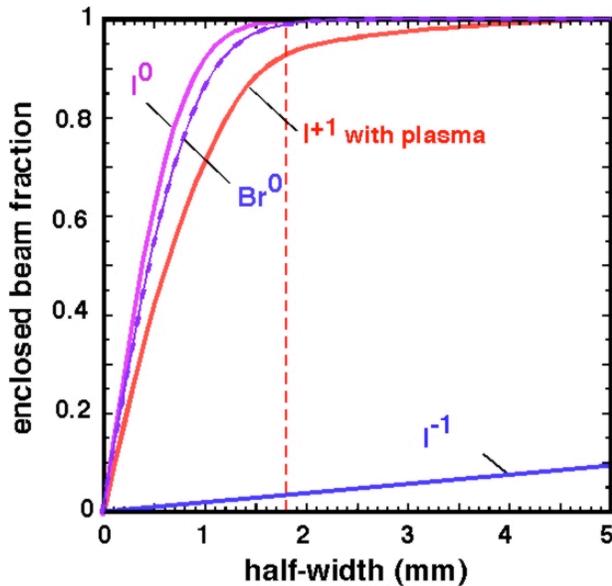


Figure 4. Enclosed beam fraction for iodine main pulses with initial charge states of -1 , 0 , and $+1$, and for a Br^0 beam. An upstream neutralizing plasma is used in the $+1$ case only. The dashed line shows the annulus half-width.

half-width band exceeds 99%, compared with 93% for the I^{+1} with a plasma. As expected, the unneutralized I^{-1} beam degrades in the entry pipe due to its own space charge, before being stripped by collisional ionization in the chamber. Figure 4 also shows results for a 1.5-GeV beam of neutral bromine (80 amu) with a particle current equivalent to 5.25 kA. Remarkably, nearly 98% of this beam is deposited in the 1.8-mm half-width band, despite the high particle current.

If negative beams of sufficient current density can be generated, transported, and photoneutralized, this improved beam deposition might permit a simpler chamber design due the absence of plasma neutralization and allow the use of beams with either higher emittance or substantially lower energy.

V. Conclusions

The beam and chamber parameters of the point design studied here reconcile the conflicting demands of accelerator cost, neutronics, final-focus, and target design for a HIF driver. The final choice of 120 beams of singly charged bismuth at 3-4 GeV is in no sense optimum, but the simulation results to date indicate that such beams could be successfully transported to a fusion target and meet the requirements on spot size and deposition history. A crucial aspect of the successful transport is the use of low-density plasma to neutralize beams before they enter the chamber.

The simulations show some flexibility in the point-design parameters. The use of ions with masses as low as that of xenon appears feasible, and the beam convergence angle can be reduced by 25% without seriously compromising the focal-spot size. Both changes might reduce the cost and complexity of a driver. In contrast, the initial beam emittance can be at most doubled before the beam focal spot becomes unusable. Some further relaxation of beam requirements might be possible if negative-ion beams of sufficient current can be accelerated and then photoneutralized after final focus.

In future simulations, we will add several features of chamber physics to the numerical model, particularly some representation of the molten-salt jets, and we will begin using more realistic distribution functions for the input beam. Multiple-beam simulations are also needed to study the possible interaction of beams near the targets. At the same time, the collaboration will continue between researchers working on the different accelerator subsystems to produce a workable physics design.

Acknowledgments

This work was performed under the auspices of the US Department of Energy by University of California Lawrence Livermore National Laboratory and Lawrence Berkeley National Laboratory under Contracts No. W-7405-ENG-48 and DE-AC-3-76SF00098.

REFERENCE

- ¹ J. LINDL, *Phys. Plasmas* **2**, 3933 (1995).
- ² M. TABAK, D. A. CALLAHAN, *Nucl. Instr. and Meth in Phys. Res. A* **415**, 75 (1998).
- ³ D. A. CALLAHAN-MILLER, M. TABAK, *Nucl. Fusion* **39**, 1547 (1999).
- ⁴ S. S. YU, *et al.*, "An Updated Point Design for Heavy Ion Fusion," Lawrence Livermore National Laboratory Report UCRL-JC-150169, (2002).
- ⁵ D. V. ROSE, *et al.*, *Nucl. Instr. and Meth in Phys. Res. A* **464**, 299 (2001).
- ⁶ D. R. WELCH, *et al.*, *Phys. Plasmas* **9**, 2344 (2002).
- ⁷ W. M. SHARP, *et al.*, *Phys. Plasmas* **10**, 2457 (2003).
- ⁸ T. P. HUGHES, *et al.*, *Phys. Rev. ST Accel. Beams* **2**, 110401 (1999).
- ⁹ D. R. WELCH, *et al.*, *Nucl. Instrum. Meth. Phys. Res A* **464**, 134 (2001).
- ¹⁰ J. D. LAWSON, *J. Electron. Control* **5**, 146 (1958).
- ¹¹ W. M. SHARP, *et al.*, *Fusion Sci Tech.* **43**, 393 (2003).
- ¹² D. R. OLANDER, *et al.*, *Fusion Sci. Tech.* **41**, 14-1 (2002).
- ¹³ C. L. OLSON, *Nucl. Instr. and Meth in Phys. Res. A* **464**, 118 (2001).
- ¹⁴ L. L. GRISHAM, *et al.*, "Proof-of-Concept Experiment for Negative Ion Driver Beams for Heavy Ion Fusion" to be published in *Proc. 2003 Part. Accel. Conf.*, 12-16 May 2003, Portland, OR.